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Chow, S. H., Diambra, A., O'Loughlin, C. D., Gaudin, C. & Randolph, M. F. (2020). Corrigendum to "Consolidation effects on monotonic and cyclic capacity of plate anchors in sand", (vol 70, pg 720, 2020). *Geotechnique: international journal of soil mechanics*, 70 (8), pp.753-753. <https://doi.org/10.1680/jgeot.19.TI.017>.

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Corrigendum

Chow, S. H., Diambra, A., O’Loughlin, C. D., Gaudin, C. & Randolph, M. F. (2020). Consolidation effects on monotonic and cyclic capacity of plate anchors in sand. *Géotechnique* 70, No. 8, 720–731, https://doi.org/10.1680/jgeot.19.TI.017. The following typographical mistakes have been identified. First, in Table 2, the first four entries in the column headed V are incorrect, as is the final footnote; the correct table is follows.

Finally, in the section headed ‘CONCLUSIONS’ (on p. 729), the sixth sentence is incorrect; the correct sentence is as follows.

Indeed, cavitation was not observed (at least adjacent to the anchor) since the maximum negative excess pore pressure was only about 20% of the theoretical cavitation.

The authors apologise to the readers of *Géotechnique* for these mistakes in the original paper.

Table 2. Centrifuge anchor test programme and results

Test series*		T : °C	μ : mPas	v : mm/s	V	q_u : kPa	N_γ	δ_u/B	α_u : deg	u_u : kPa	$\Delta z_t/B$
Dry [§] ($\gamma' = 16.43 \text{ kN/m}^3$) (Chow <i>et al.</i> 2015)	M0-1D	—	0	1	—	728.4	8.9	2.96	66.8	—	—
	IC1D	—	0	3	—	825.2	10	2.65	63.8	—	—
	IC1-25D	—	0	3	—	820.3	10	2.94	66.3	—	—
	IC1-5D	—	0	3	—	712.0	8.7	2.75	62.1	—	—
S1 (water), $\gamma' = 10.32 \text{ kN/m}^3$, $c_v = 4.93 \times 10^{-4} \text{ m}^2/\text{s}$ at $z = 2.8 \text{ m}$	M0-3W(1)†	—	1	0.3	0.02	445.7	8.6	4.41	—	—	—
	M0-3W(2)	—	1	0.3	0.02	439.8	8.5	4.11	55.3	65.1	2.67
	IC1W	—	1	30	1.95	583.7	11.3	3.70	47.3	75.3	1.65
	IC1-25W‡	—	1	30	1.95	509.9	9.9	3.88	52.8	64.9	1.56
S2 (methocel), $\gamma' = 10.23 \text{ kN/m}^3$, $c_v = 7.3 \times 10^{-7} \text{ m}^2/\text{s}$ at $z = 2.8 \text{ m}$	M30M	19.2	743	30	1349	1201.7	23.5	5.02	54.7	12.8	2.90
	IC1M	20.3	707	30	1276	1529.2	29.9	4.94	53.4	0.5	2.66
S3 (methocel) $\gamma' = 10.53 \text{ kN/m}^3$, $c_v = 5.99 \times 10^{-7} \text{ m}^2/\text{s}$ at $z = 2.8 \text{ m}$	M0-3M	21.1	675	0.3	16	687.1	13.1	4.03	52.3	51.6	2.47
	M1M	20.4	703	1	55	802.9	15.3	4.34	52.3	41.6	2.88
	M3M	21.1	678	3	158	1067.0	20.3	5.11	53.7	18.1	2.60
	M10M(1)‡	20.9	684	10	533	1552.7	29.5	6.27	60.1	−12.3	2.74
	M10M(2)‡	20.6	693	10	540	1522.8	28.9	6.05	59.7	−19.1	2.56
	M30M‡	20.9	682	30	1595	1497.6	28.5	5.99	59.7	−9.7	2.48

*For ease of reference, tests are identified as $LvP(n)$, where

(a) ‘ L ’ denotes the loading type (M for monotonic loading, IC for irregular cyclic loading)

(b) ‘ v ’ denotes the monotonic loading rate ($v = 0.3$ to 30 mm/s) or the peak cyclic load ratio ($\text{CLR}_{\text{peak}} = q/q_u = 1$ or 1.25)

(c) ‘ P ’ denotes the pore fluid (D for dry, W for water, M for methocel)

(d) ‘ n ’ denotes the test recurrence (‘1’ for the first test, ‘2’ for the second test etc.).

†PPT and/or accelerometer data lost due to damaged cable.

‡Test stopped due to actuator hitting displacement limit.

§Drained monotonic and cyclic test results for a plate anchor with similar geometry (except $t_a = 2.75 \text{ mm}$) in dry dense sand.