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Strain-dependent photodetection with layered InSe photoconductors

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Abstract

Controlled bandgap modulation is of particular interest for next generation optoelectronic devices, allowing the development of 'active' or 'reconfigurable' detectors and emitters. In van der Waals layered semiconductors, which exhibit high strain tolerance, strain has become a notable tool for active bandgap tuning. In this work, we demonstrate a flexible bulk InSe gated photoconductor with strain-induced modulation of the bandgap energy, shifting to higher and lower energies under compression and tension, respectively. Photoluminescence measurements reveal shift rates of around $117.1 \text{ meV}\cdot\%^{-1}$ in tension, and $107.6 \text{ meV}\cdot\%^{-1}$ in compression. Spectral responsivity measurements indicate smaller shift rates, likely due to non-uniform strain application. Notably, these flexible devices achieve impressive performance with specific detectivities up to $3.78\times 10^{12} \text{ cm}\cdot\text{Hz}^{1/2}\cdot\text{W}^{-1}$, a rise time of $4.1 \text{ }\mu\text{s}$, and a responsivity of $1.25\times 10^3 \text{ A}\cdot\text{W}^{-1}$. The realisation of high responsivity and fast response times underscores the potential of this device architecture for advanced optoelectronic applications.

Van der Waals (vdW) materials, such as transition metal dichalcogenides and graphene, have emerged as promising candidates for optoelectronic applications [1-5]. Their appeal largely stems from their unique properties such as strong optical absorption and near-unity photoluminescence quantum yields [6, 7], particularly in monolayer and few-layer forms [8]. A less explored sub-set of vdW materials, the III-VI vdW semiconductors GaSe and InSe, retains excellent optoelectronic properties even in their bulk form. InSe, in particular, has gained significant interest due to its scalable growth [9, 10], high photoluminescence quantum yield [11], ballistic transport [12], and second-harmonic generation [13].

The bandgap of InSe varies from an indirect ~ 2.4 eV gap in its monolayer form, to a direct ~ 1.3 eV gap in its bulk form, making it a promising candidate for visible to near infrared (NIR) optoelectronic applications [14, 15]. Bulk InSe photodetectors have already demonstrated high responsivities, reaching up to $10^8 \text{ A}\cdot\text{W}^{-1}$, at $\lambda = 450 \text{ nm}$ [16-18]. Additionally, the bandgap of bulk InSe can be actively tuned via the application of strain. Studies on flexible substrates have shown that its peak photoluminescence (PL) emission can be reversibly redshifted by $57\text{-}154 \text{ meV}\cdot\%^{-1}$ under tensile strain [19, 20], and blue-shifted by $100\text{-}140 \text{ meV}\cdot\%^{-1}$ under compressive strain [20]. This strain-tunability has been leveraged to develop photodetectors with adjustable spectral response and responsivity [21, 22]. However, as shown in Table 1, flexible InSe-based devices have yet to match the performance of devices formed on rigid substrates, particularly at the band edge of bulk InSe. The table summarizes key performance metrics for a selection of flexible vdW material photodetectors measured under strained conditions.

In this work, we demonstrate a strain-tunable InSe gated photoconductor on a flexible substrate, achieving a highest-in-class responsivity of $1.25 \times 10^3 \text{ A}\cdot\text{W}^{-1}$ and a fast rise time of $4.1 \mu\text{s}$, setting a benchmark for flexible bulk InSe photoconductive devices. We quantify the strain-induced band edge shifts using PL and spectral photoresponse measurements, observing shift rates up to $117.1 \text{ meV}\cdot\%^{-1}$ under tensile strain and $107.6 \text{ meV}\cdot\%^{-1}$ under compressive strain. These results highlight the substantial potential of strain-tuneable bulk InSe-based optoelectronics.

Gamma-phase InSe has a rhombohedral layered structure with a $R3m$ space group, as shown in Fig. 1a. The bandgap of this material undergoes broadening (narrowing) under compressive (tensile) strain, as verified in experiments [20, 23], and through simulations (see Supporting Information S1). To experimentally test the magnitude of this strain-dependent behaviour, we first measure InSe's PL as a function of strain. We utilise bulk InSe flakes (2Dsemiconductors, Bridgman growth) with an average optical lifetime of 9.4 ns , and thicknesses ranging between $50\text{-}300 \text{ nm}$ (see Supporting Information S2 and S3). This thickness range was chosen to

maximise light absorption in later photoconductive devices (see Supporting Information S4). Previous studies have also concluded that InSe's strain dependent band gap shift begins to saturate at bulk thicknesses above ~ 20 nm [20], and that for bulk InSe flakes of ~ 100 nm the binding energies are lower than the thermal energy at room temperature, indicating a free carrier dominated system [11]. The bulk flakes used in this study are mechanically exfoliated from a bulk crystal, onto a $1\text{ }\mu\text{m}$ thick polymethyl methacrylate (PMMA) film which is layered onto the surface of an 0.8 mm polyimide substrate. PMMA is used to ensure good strain transfer efficiency [23, 24]. Strain is applied to the substrate and InSe flake via a two-point bending method, as shown in Fig. 1b. This method has been used in similar studies in the past [25-27], however, some limitations have been reported including slippage between the 2D material and the substrate [24], and uncertainty as to the onset of strain application. To address these limitations, we used calculated strain values at 0% and $\sim 0.8\%$ strain to extract the shift rates, as we find this to be the most accurate region (see Supporting Information S5).

To probe the change in the bandgap with strain, the PL of multiple flakes were measured between 0% to 1% , taken using a Horiba Synapse InGaAs/Symphony system with a $\lambda = 785$ nm illumination laser. Representative PL spectra are provided in Fig. 1c for tensile strain with the unstrained PL peak position centred around 1.26 eV, in line with previous studies [20, 23]. The shift rate in the PL peak position under tensile strain is found to be $74.4 \pm 2.1\text{ meV}\cdot\%^{-1}$ in a redshift direction. The repeatability of this behaviour is confirmed in Fig. 1d, in which 0.7% tensile strain was applied to a representative sample 100 times, with the PL being captured after every tenth application of strain. Fig. 1e shows the PL spectra of a representative InSe flake as a function of compressive strain ranging between 0% to 1% , with a resultant blueshift of $93.0 \pm 3.1\text{ meV}\cdot\%^{-1}$.

To support these results, Fig. 2a shows the experimentally observed peak shift with tensile strain from the centre of several randomly oriented and different thickness bulk InSe flakes. It shows that the peak shift is relatively consistent and does not depend heavily on the angle between the bending axis and InSe's crystal orientation. From these measurements, the average shift rate under tensile strain is $84.6\text{ meV}\cdot\%^{-1}$, with values between $74.4\text{ meV}\cdot\%^{-1}$ and $117.1\text{ meV}\cdot\%^{-1}$ measured from different flakes, agreeing with ranges reported in literature of $57\text{-}154\text{ meV}\cdot\%^{-1}$ [19, 20].

Further PL investigation was performed using hyperspectral imaging on a representative thick InSe flake (shown in Fig. 2b), to understand how the entire flake is influenced by strain. These measurements were taken using a Photon Etc. IMA hyperspectral imaging system including a ZephIR 1.7 InGaAs camera and a $\lambda = 463$ nm diode laser illumination source. Fig. 2c shows the PL peak position map across this flake, showing a substantial variation in local strain

across the flake under both compressive and tensile strain. At 0% strain, there is a mostly uniform PL peak across the entire flake, with emission close to the bulk unstrained InSe PL emission of 980 nm (1.26 eV). At both -1% and 1% strain, the edges of the flake retain values near the unstrained PL emission peak, whilst the centres of both images show strong shifts. These centres are at $\lambda = 900$ nm (shift rate of $107.6 \text{ meV}\cdot\%^{-1}$ from -0.8% to 0%) for compressive strain and $\lambda = 1040$ nm (shift rate of $89.0 \text{ meV}\cdot\%^{-1}$ from 0% to 0.8%) for tensile strain. The tensile PL peak positions from the centre of the flake are also included in Fig. 2a. The underlying mechanism for the regionality of the strain is likely associated with incomplete adhesion to the substrate at the flake edges [28]. Notably, at the boundary of the flake there is additional broader PL emission resulting from the sample's emission outcoupling to the flake edge. An accompanying mapping of InSe's A^1_{1g} , A^2_{1g} and E^1_{2g} Raman peaks across another bulk flake, showed shift directions under strain consistent with previous reports, but did not provide enough resolution to distinguish regional variation (see Supporting Information S6).

Next, to investigate the impact of strain on InSe photodetection in the NIR we fabricate gated photoconductors on flexible substrates, a device schematic of which is shown in Fig. 3a. The InSe photoconductors were fabricated on polyimide sheets with a thickness of 0.8 mm. Shadow masks were used to define source, drain and gate contacts. The gate contact consisted of a stack of Ti (5 nm) and Ni (60 nm) deposited via electron-beam and thermal evaporation, respectively. A PMMA (1 μm) gate insulator was subsequently spin-coated and cured onto the substrate followed by mechanical exfoliation of the InSe channel, and then thermal evaporation of the Ni (80 nm) source/drain contacts. Ni was chosen as it adhered well to the PMMA surface and produced consistent Ohmic contacts to InSe. These contacts also influence how strain is transferred to the material as the flake is fixed to the substrate at the Ni contacts. Fig. 3b shows an optical microscope image of a representative device highlighting the areas of InSe (red) and Ni (blue). Fig. 3c shows an atomic force microscope (AFM) topological image of the edge of this flake, where the step-height was ~ 270 nm, as plotted in Fig. 3d.

Following fabrication, the devices were electrically characterised with a Keysight B1500A semiconductor device parameter analyser by measuring the drain current (I_D) versus gate voltage (V_G) and I_D versus drain voltage (V_D) behaviour. Fig. 3e shows the I_D - V_D characteristic of a representative device and how the Ni front electrodes were able to form Ohmic contacts with the InSe flake. Fig. 3f shows the I_D - V_G behaviour in both the dark (dashed lines) and in the light (solid lines) when illuminated with a visible light lamp ($\sim 10 \text{ mW}\cdot\text{cm}^{-2}$). Clear n-type behaviour can be seen with the dark current reaching a minimum at higher negative gate voltages. Furthermore, an on/off ratio of $\sim 10^6$ was measured in dark conditions when biased at $V_D = 100 \text{ mV}$.

To analyse the InSe photoconductor's performance, representative devices were characterised under modulated $\lambda = 685$ nm and $\lambda = 980$ nm laser illumination. The device's photoresponse was captured, after amplification via a transimpedance amplifier (SR570), on an oscilloscope. The InSe photoconductor's photoresponse speed, shown in Fig. 4a, displays a rise time of 4.1 μ s and a fall time of 10.2 μ s with illumination from a modulated $\lambda = 639$ nm laser, corresponding to an RC limited bandwidth of ~ 34 kHz. These rise/fall times were measured between 10-90% of the on/off current when biased at $V_D = 100$ mV and no V_G applied. These results are among the fastest response times reported in the literature for InSe photodetectors [21, 29]. The intensity dependent responsivity and detectivity were next investigated at $\lambda = 639$ nm. The responsivity values were calculated from the measured photocurrent divided by the incident light intensity. Where the incident power was determined using a calibrated germanium detector (FDG03-CAL) with known responsivity. Detectivity was calculated by using the estimated shot noise from the measured dark current (see Supporting Information S7). These measurements, shown in Fig. 4b, are taken at differing gate biases ($V_G = -40$ to 40 V) with a constant $V_D = 100$ mV. At a gate voltage of $V_G = 20$ V, the highest responsivity of 1.25×10^3 A $\cdot$ W $^{-1}$ was measured at an incident power of 767 nW $\cdot$ cm $^{-2}$. The magnitude of the responsivity confirms the presence of gain, which is discussed in Supporting information S8. A maximum specific detectivity of 3.78×10^{12} cm $\cdot$ Hz $^{1/2}$ $\cdot$ W $^{-1}$ was achieved under these same conditions. We note that this detectivity should be taken as an upper limit estimate due to utilising the calculated shot noise from the device's dark current. In reality, 1/f noise can also contribute to the noise behaviour of photoconductive devices, particularly at low frequencies [30, 31]. However, at frequencies close to the bandwidth of InSe the shot noise is found to be a reasonable estimate of total noise (see Supporting Information S7). Regardless, these results compare well to other flexible devices in the recent literature, showing the highest responsivity and detectivity values compared to other InSe based flexible devices [21, 22]. The improved responsivity is partially attributable to the increased absorption due to the use of thicker InSe photoabsorbers relative to previous studies. The decrease in responsivity with increasing illumination intensity is common for nanomaterial detectors and has been explained by the saturation of trap states, which affects the photoconductive gain [18, 32-38]. The exception to this behaviour, seen for strong negative gate biases, may be associated with the gate and injection dependence of quantum efficiency/gain within the InSe absorber [39, 40]. Another set of measurements, shown in Fig. 4c were taken under $\lambda = 980$ nm illumination, which is close to InSe's unstrained band edge. The best responsivities and detectivities obtained at $\lambda = 980$ nm were 89 A $\cdot$ W $^{-1}$ and 2.71×10^{11} cm $\cdot$ Hz $^{1/2}$ $\cdot$ W $^{-1}$, respectively, both of which were measured under low intensity (2.2 μ W $\cdot$ cm $^{-2}$) with $V_G = 20$ V. This lower responsivity at $\lambda = 980$ nm versus $\lambda = 639$ nm is likely a consequence of InSe's lower absorption coefficient at its band edge (see Supporting Information S8).

This lower absorption/photoresponse around the band edge can be modulated with strain, and as such we next measured the strain-dependent spectral responsivity. Representative devices were measured on a custom-built dispersive visible-NIR characterisation platform (see Supporting Information S8). Figure 5a and 5b show the changes in normalised spectral responsivity as a function of tensile/compressive strain for two devices, with the black curves being representative of 0% strain in both plots. Normalisation was performed using the peak value within the range of 1.2-1.3 eV, although only minor changes in the global photoresponse magnitude are noted without normalisation (see Supporting Information S9). In Fig. 5a, devices are measured under tensile strain ranging from 0% to 1.1%, operating with $V_G = 20$ V. A clear redshift in the band edge can be seen with increasing tensile strain, with a shift rate of $44.5 \pm 1.5 \text{ meV} \cdot \%^{-1}$. The bandgap was estimated by making fits to the external quantum efficiency (EQE) band edge using a previously reported technique [41]. In addition to the translation of the band edge position to lower energy values, a reduction in the gradient of the band edge was also seen under strain values above 0.8%. This may be due to different regions of the device exhibiting different absorption behaviour due to non-uniform strain. The inset of Fig 5a shows the enhancement in responsivity as a function of wavelength when switching between 0% and 1% strain, with a peak enhancement around 1.1eV. At this wavelength, the photoresponse is enhanced by almost two orders of magnitude, demonstrating effective photoresponse modulation. In Fig. 5b, devices were measured under compressive strain with a floating back gate and $V_D = 500 \text{ mV}$. A minor blueshift is seen with a band edge shift rate of $35.1 \pm 4.6 \text{ meV} \cdot \%^{-1}$. The smaller strain rates relative to the earlier PL analysis is likely at least partially due to non-uniform strain effecting the spectral responsivity (which collects current from the entire device) to a greater degree than the PL measurements (which samples a smaller region of a given flake).

Another representative device was used in Fig. 5c for repeatability testing of the InSe photoconductors under multiple cycles of tensile strain. The device was strained from 0% to 0.7% 1000 times, showing very consistent responsivity up to 800 cycles. The spectral responsivity drops after 900 cycles, due to visible damage to the metal contacts, which could be improved by using different contacting schemes. Regardless, this test demonstrates the durability of the InSe photoconductor's responsivity even without consideration for device longevity. Multiple strategies could be implemented to improve device endurance, and strain uniformity. Encapsulation may help by protecting the contacts, enhancing strain uniformity, limiting oxidation, and preventing wrinkling of the InSe. Similarly, the use of adhesion promoters, such as (3-aminopropyl)triethoxysilane or poly-L-lysine, could also be used to improve flake adhesion and strain uniformity. Another issue relevant to InSe, is surface oxidation which can lead to performance degradation for thin devices [42]. However, given the

focus on thick InSe photoabsorbers in this study, and the fact that InSe's surface oxide can be made self-limiting [43], we do not anticipate this to be a major problem (see Supporting Information section S10).

Finally, Fig. 5d summarises the results of this study, plotting the estimated bandgap extracted from the PL and spectral responsivity measurements. All datasets show a clear trend of increasing/decreasing bandgap energy with compressive/tensile strain. As discussed above, the lower strain rates seen from spectral responsivity measurements is likely a consequence of being large area measurements, and that more uniform strain application could improve the observed band edge shift. Regardless, these results demonstrate effective modulation of the band edge and show promise for the future of strain tuneable bulk InSe optoelectronic devices for visible to NIR applications. This includes use for single pixel spectroscopy by leveraging the changing photoresponse profile with respect to strain to perform spectral reconstruction around InSe's band edge [44]. Switching to miniaturised strain application platforms, such as by using arrays of micro-electro-mechanical actuators, could also introduce other applications, such as reconfigurable imaging.

This study investigated the effect of strain on InSe's bandgap through PL peak position and spectral responsivity measurements. PL measurements revealed significant PL peak position shift rates of $117.1 \text{ meV}\cdot\%^{-1}$ under tension and $107.6 \text{ meV}\cdot\%^{-1}$ under compression. Spectral responsivity measurements, taken on gated, flexible InSe photoconductors, showed smaller band edge shift rates of $44.5 \text{ meV}\cdot\%^{-1}$ and $35.1 \text{ meV}\cdot\%^{-1}$ for tensile and compressive strain, respectively. These flexible InSe photoconductors devices exhibited visible wavelength responsivity up to $1.25\times 10^3 \text{ A}\cdot\text{W}^{-1}$, specific detectivity up to $3.78\times 10^{12} \text{ cm}\cdot\text{Hz}^{1/2}\cdot\text{W}^{-1}$, and rise and fall times of $4.1 \text{ }\mu\text{s}$ and $10.2 \text{ }\mu\text{s}$, respectively. Representative devices were also shown to maintain similar performance after 800 strain cycles. These results highlight the potential of strain tuneable InSe photoconductors for visible and NIR detection, paving the way for flexible and reconfigurable optoelectronic applications.

Supporting Information

DFT bulk-InSe bandgap simulations; InSe lifetime measurements; AFM thickness measurements; thickness dependent absorption simulations; profilometry measurement of strain to determine application method accuracy; Raman mapping of InSe under strain; detectivity calculations and noise current spectral density measurements; spectrally dependent responsivity, external quantum efficiency (EQE), absorption, and gain profiles; non-normalised strained responsivity spectra; InSe air exposure measurements.

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Conflicts of interest

The authors declare no conflict of interest.

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Figures

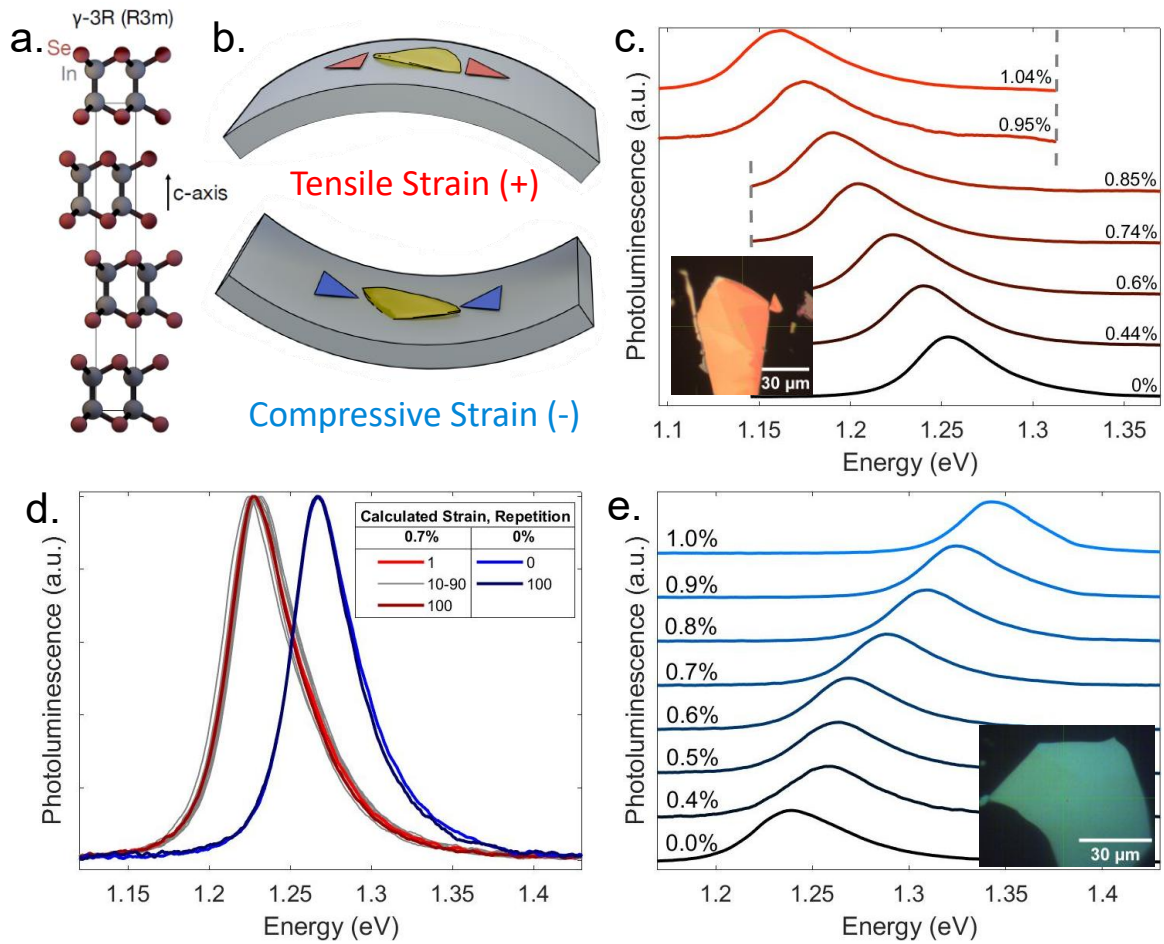


Figure 1: Strain application to bulk γ -InSe, (a) side-on view of γ -InSe crystal structure. (b) Schematic of how tensile and compressive strain are applied to the InSe flake (yellow). (c) Photoluminescence of bulk InSe under tensile strain from 0% to 1.04% calculated strain. The grey dashed lines in (c) mark the edge of the window for the PL measurement. (d) Photoluminescence at 0% and 0.7% tensile strain over 100 strain repetitions with blue curves at 0% strain and red curves at 0.7% tensile strain. (e) Photoluminescence of bulk InSe under compressive strain from 0% to 1% calculated strain. Inset in (c) and (e) are images of the InSe flakes measured, with a scale bar of 30 μ m.

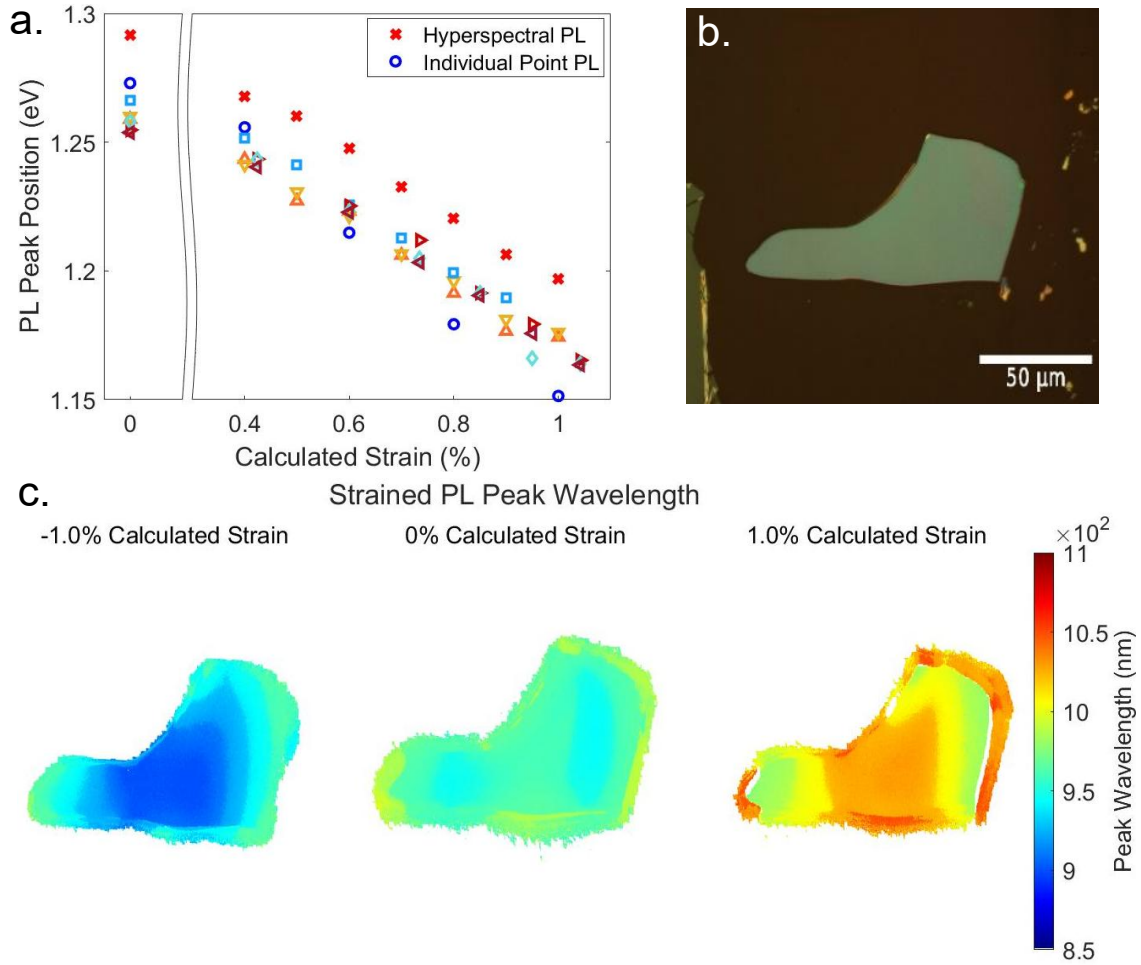


Figure 2: Additional photoluminescence characterisation under strain. (a) Collection of tensile strain PL peak position measurements from various bulk InSe samples along with the PL peak position from the hyperspectral measurement. Solid x-marker is for hyperspectral measurement and hollow markers are for all individual point measurements. (b) Optical microscope image of the InSe flake measured in (c). (c) Hyperspectral PL images of an InSe flake at -1%, 0%, and +1% strain. Colour represents PL peak emission wavelength.

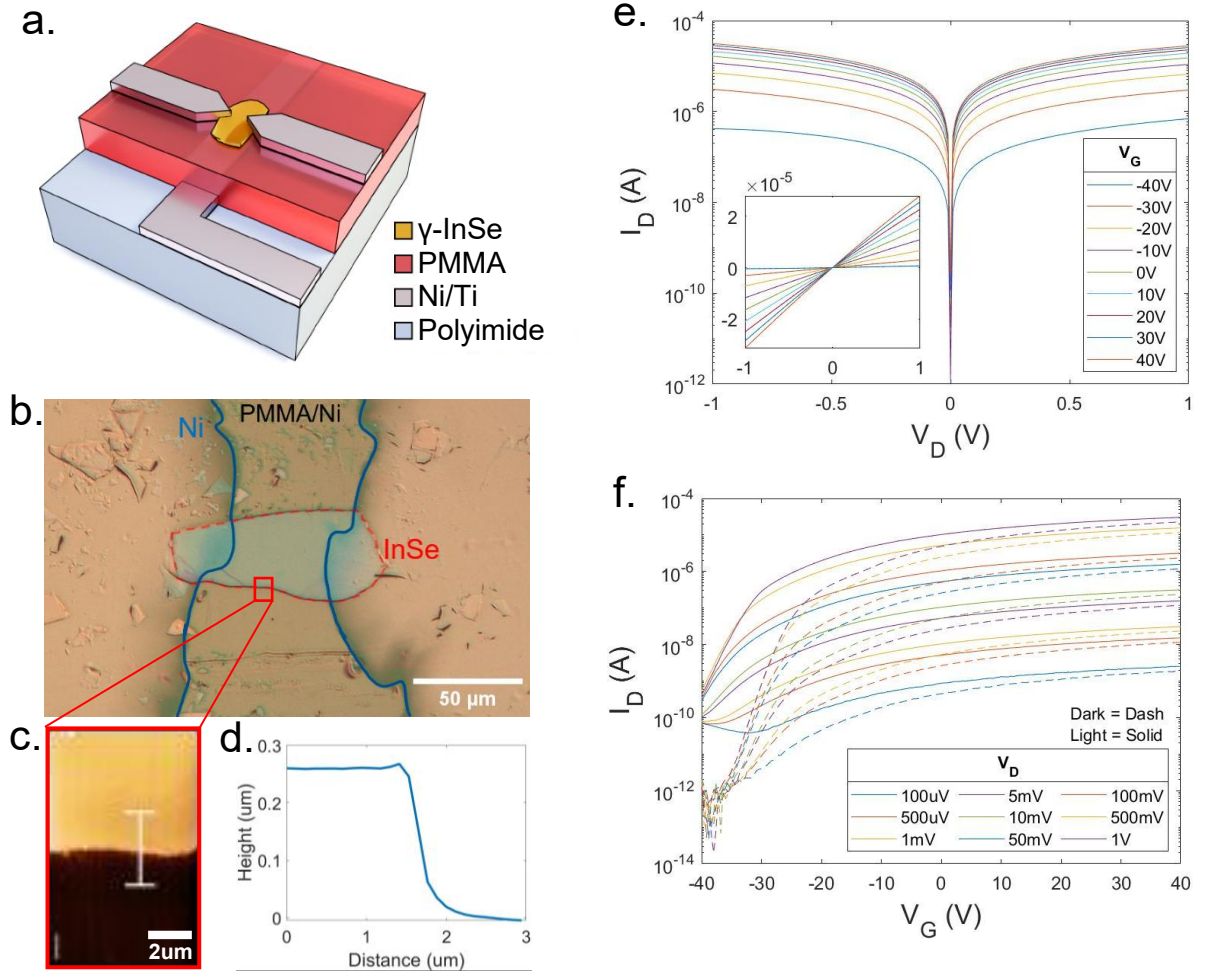


Figure 3: (a) Schematic of a gated InSe photoconductor device. (b) Optical microscope image of a representative InSe device, with a scale bar of 50 μm . (c) AFM topography of the highlighted area in (b), with a scale bar of 2 μm , and the height profile in (d) is extracted from white line in the image with the width of the line representing the area which the height profile is averaged across. (e) and (f) log scale plots of I_D vs. V_D and V_G respectively. Inset in (e) shows the same data on a linear scale showing linear behaviour. (f) also includes the I_D with no illumination and $\sim 10 \text{ mW cm}^{-2}$ white light illumination on the sample.

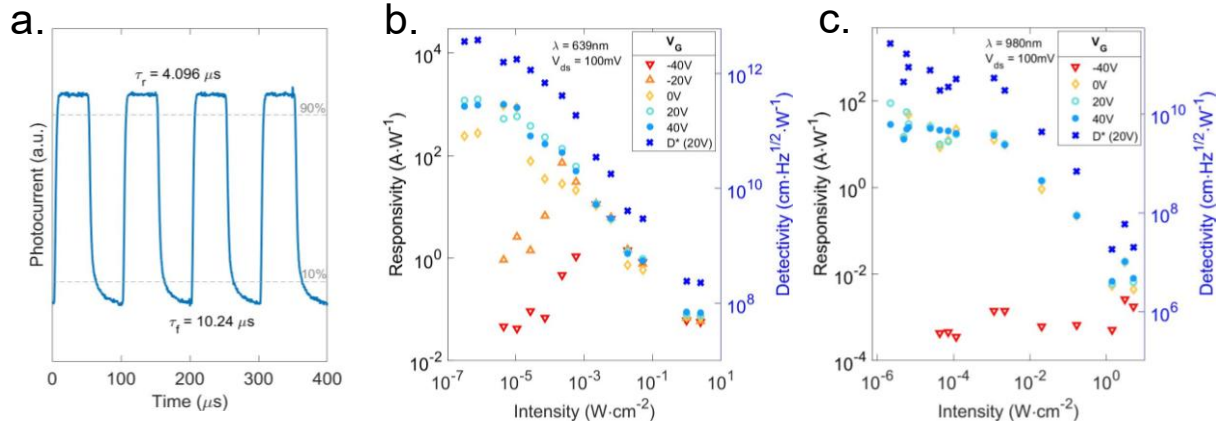


Figure 4: Photoconductor characterisation, (a) Measured unstrained photoresponse under $\lambda = 639\text{ nm}$ illumination modulated at 10 kHz and the device biased with $V_D = 100\text{ mV}$ and no V_G applied. Unstrained responsivity and detectivity measurement with an excitation source of $\lambda = 639\text{ nm}$ (b) and $\lambda = 980\text{ nm}$ (c) for varying illumination intensity. The gate bias was adjusted from -40 V to $+40\text{ V}$. The detectivity was only determined at $V_G = +20\text{ V}$ (dark blue crosses). All measurements were taken at room temperature with $V_D = 100\text{ mV}$.

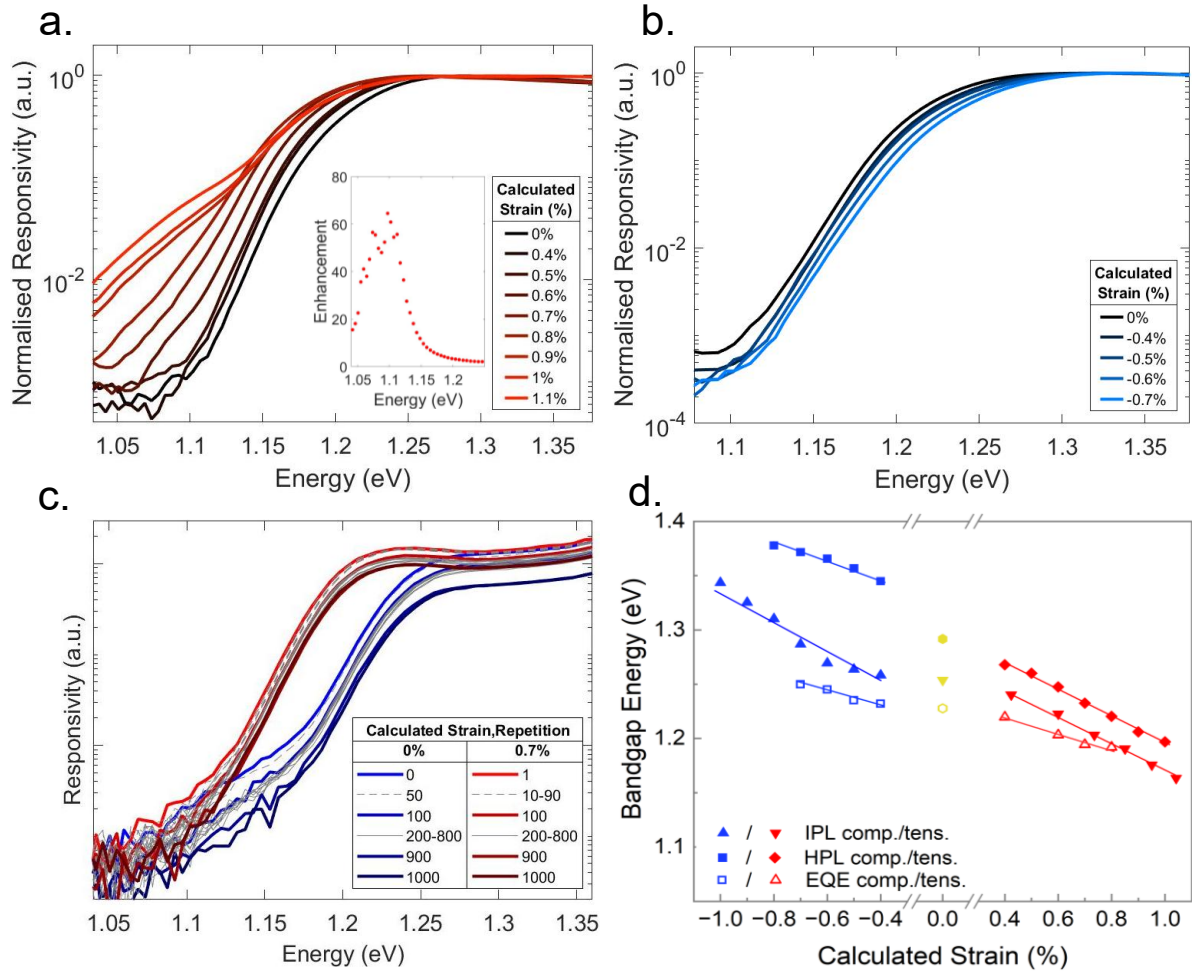


Figure 5: Spectral response measurements of representative strained InSe photoconductors. (a) and (b) show tensile and compressive strain from 0% to 1.1% and 0% to -0.7% respectively. Inset in (a) shows the enhancement in responsivity when switching from 0% to 1% tensile strain near the band edge. (c) Repeatability testing of tensile strain from 0% (blue lines) to 0.7% (red lines) over the course of 1000 strain repetitions (grey lines show all measured spectra at both strain values). (d) Collection of hyperspectral PL peak position (HPL, solid squares/diamonds), extracted bandgap from EQE measurements (PC, hollow shapes), and a representative tensile and compressive individual point PL (IPL, solid triangles). Compression = blue and tensile = red in PL and EQE measurements. Lines provide a guide to the eyes only.

Table 1: 2D material strain tunable photoconductors

*Substrate: PC (polycarbonate), PET (Polyethylene Terephthalate), PETG (Polyethylene Terephthalate Glycol), PI (Polyimide)
^Shift Rate: T (Tensile), C (Compression), PD (Photodetector), PL (Photoluminescence)

Material	Substrate*	Measurement Wavelengths (nm)	Bias (V)	Responsivity (A·W ⁻¹)	Detectivity (cm·Hz ^{1/2} ·W ⁻¹)	Response Time (s)	Maximum Strain (%)	Shift Rate^ (meV·% ⁻¹)	Ref.
MoS ₂	PC	400-700	1	5×10 ⁻³	-	~4	0-1%	T: 51 (PD)	[45]
MoS ₂	PC	450-800	10	200	-	80×10 ⁻³	-1.44 - 0.48%	135 (PD)	[46]
WSe ₂ Homojunction	PET	500-850	0	0.280	1.3×10 ¹²	34×10 ⁻³	0 - 1.04%	-	[47]
WS ₂ Homojunction	PET	600	0.5	44.8	1.12×10 ¹³	-	0 - 0.98%	-	[48]
ReS ₂	PI	830	0.1	11.3	1.7×10 ¹⁰	-	0 - 0.25%	-	[49]
bP	PETG	1300-5500	0.1	~2.8	8.45×10 ⁹	18.7×10 ⁻⁶	-0.66 – 1.21%	162 (PL) T: 157 (PD)	[25]
InSe	PET	400-800	0	0.825	1.7×10 ¹²	20.3×10 ⁻⁶	0 - 0.62%	-	[21]
InSe	PET	254-700	5	115.9	-	30×10 ⁻³	0-1.06%	T: 58 (PL)	[22]
InSe	PET	840-1100	0.3	-	-	-	-0.62 - 1.06%	T: 154 (PL) T: 64 (PD) C: 140 (PL)	[20]
InSe	PI	639-1200	0.1	1.25×10 ³	3.78×10 ¹²	10.2×10 ⁻⁶	-1 - 1.1%	T: 117.1 (PL) T: 44.5 (PD) C: 107.6 (PL) C: 35.1 (PD)	This Work

TOC Graphic

